

A new strategy to improve the stem sealing

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How to counter the usual valve packing relaxation

The current experimental and operative evidences show that the stem graphite sealing incurs a gradual relaxation that comes in the first weeks of work and after the first thermal cycle. A better knowledge of the product and some simple precaution can mitigate this effect with improved performance.





A graphite stem packing is composed ususally by dieformed flexible graphite rings and die-formed braided packing rings in different shape and combinations





Among the main technical specification for the packing qualification is recommended to refer to the ASTM F2191 and ASTM F2168 which qualify in details the main graphite yarns and the graphite foil attributes, introducing the correct terminology and classification terms because "High Carbon content, Great chemical resistance in the range 0 ÷ 14 except the strong oxidizing and Great **resistance to the high Temperature**" (the most famous attributes) could be insufficient to qualify the right graphite sealing.



ASTM F 2191: the packing classification

- Type yarns morfology
- Class level of detrimental material

• Grade inhibitor of corrosion (Y or N)



Yarns morfology

- Type I—Continuous carbon or graphite yarn.
- Type II—Staple carbon or graphite yarn.
- Type III—Braided flexible graphite.



Type I and Type II





BCF: Bulked Continuous Filament Yarns

PAN yarns with thousand of continuous fibers

Staple Yarn: Discontinuous Filament Yarns

PAN or Rayon yarns with milion of discontinuous staple fibers



Oxidized PAN Fibers



Type I and Type II

Continuous carbon or graphite yarn - Staple carbon or graphite yarn.

- PAN Polyacrylonitrile
- Viscose Rayon





Type III - Flexible Graphite Strands



1 -Flake



3 - Strands



4 - Flexible Graphite Packing

2 - Foil

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The diagram shows the relationship within Thermal Conductivity and Young's Module of different materials. The recovery's gap it's dramatically evident.





The graphite Packing offers different behavior due to the different graphite yarns properties



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Information about the graphite stem packings

Class – Level of detrimental material

TABLE 2 Detrimental Materials

Element	Maximum Allowable Total Impurity Levels in parts per million (ppm)
Mercury (Hg)	10
Sulfur (S)	750
Total halogens (chlorine, bromine, and fluorine)	500
Chlorine (CI)	250
Bromine (Br)	250
Fluorine (F)	250

Class 1—For use where detrimental material and lubricant content of the packing need not be controlled beyond normal manufacturing limits. **Class 2**—For use where detrimental materials content must be controlled to limits specified herein. **Class 3**—For use where detrimental materials content need not be controlled beyond normal manufacturing limits, and media temperatures do not exceed 500°F (260°C).



Grade – Inhibitor of corrosion (Y or N)

Grade A—Treated with corrosion inhibitor.

(Zinc powder or barium molybdate)

Grade B—Without corrosion inhibitor.





The involved parameters

- Radial stress 6i conversion factors for wich
 - 6ri = Ci 6a
 - бro = Со ба
- Gland load
- Coefficient of friction
- Rings number



The recent finite element analysis (FEA) indicates that the ratio Ci/Co tends to 1 independently to the load and the vertical position across the stem. This result integrates the others experimental analysis for which this convergence comes after the load of 25 Mpa.



Source: MPA - Characteristics and Testing Technique for stuffing Box Packing



The FEA allows to analyze the value Ci in correlation between the gland stress, the coefficient of friction and the rings number. It seems that Ci is weakly sensitive to the friction, increases with the rings number and, surprisingly, decreases with higher load. The coefficient appears insensitive to the packing relaxation.





The coefficient of friction is not constant and decreases for higher load. The difference between the braided packing and the flexible graphite die-formed rings is minimal



Source: MPA - Characteristics and Testing Technique for stuffing Box Packing



The compression curve (rif: stem packing 6 rings, 2 braided wiper and 4 die-formed flexible graphite rings), shows that the lost deformation is around 15%. It should be appropriate improves the packing installation procedure for a better sealing behavior.





The radial compressive stress decreases along the stem and the stuffing box room.

The gap between the Top and the

Bottom rings depends also to the number of ring which composes the sealing kit.





The radial compressive stress curve changes because:

- Material Relaxation
- Thermal cycles
- Machanical Cycles

Radial stress distribution line

The eveidence is in the needed to re-tighten the packing σ_{T}



In order to reduce this effect and armonize the compressive stress curve it is possible to introduce in the system a convex bushing which push up the packing from the bottom.





The better and enhanced compressive stress in the bottom rings improves the sealing and offers reliable self adjustements which reduce the relaxation troubles and the valve actuation effect.





Any disadvantage occurs in the use of a convex bushing if the clearances are in accordance to the standard specifications. The effectiveness of the convex bushing grows faster both in association with the surface than with the pressure





Conclusions

The introduction in the system of the new element does not solve the regression problem in the small valves (rating 150 lbs) even if some benefit is detectable.

In the medium and big sized values, the effect of the bottom force becomes more and more evident, improving the efficiency of the sealing starting from the 150 lbs rating.

From 2.500 psi rating and upper, the evidence of the bottom force is considerable and changes the quality of the sealing reducing also the actuation stress.



Conclusions

The introduction in the system of the new element does not solve the regression problem in the small valves and basic rating 150 lbs even if some benefit is detectable.

In the medium and big sized values, the effect of the bottom force becomes more and more evident, improving the efficiency of the sealing starting also from the 150 lbs rating.

From 2.500 psi rating and upper, the evidence of the bottom force is considerable and changes the quality of the sealing reducing also the actuation stress.



THANK YOU

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